

# Y-12

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Y-12  
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AIRFIL: A FORTRAN PROGRAM FOR REDUCTION OF  
DATA OBTAINED FROM ALPHA SPECTROMETRY  
OF PERIMETER AIR FILTERS

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AIRFIL: A FORTRAN PROGRAM FOR REDUCTION OF DATA OBTAINED  
FROM ALPHA SPECTROMETRY OF PERIMETER AIR FILTERS

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INSEPT A

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ABSTRACT

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Starting in the mid 1970s,

Isotopic alpha spectrometry of  $^{238}\text{U}$ ,  $^{235}\text{U}$ , and  $^{234}\text{U}$ , along with gross alpha/beta counting of perimeter air filters, is performed by the Oak Ridge Y-12 Plant Laboratory in support of the Environmental Monitoring Section of the Radiation Safety Department. Weekly samples are gross alpha/beta counted and the isotopic analysis performed on quarterly composites.

Calculations and data management represent a major portion of the analysis time when performed manually, even with a desktop calculator. In order to reduce calculation time, perform orderly data manipulation and management, reduce errors due to redundant calculations, and eliminate report typing turnaround time, a computer program (AIRFIL) has been developed that performs these functions. The program accepts data through user prompts, then calculates and prints intermediate and final data, including detection limits.

of air concentrations are set up to the plant lab. (Hinton, 1984).

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## SUMMARY

A FORTRAN program (AIRFIL) has been written to manage raw counting data obtained from perimeter air filters. The program reduces calculation time from hours to only a few minutes, while reducing the possibility of human error. Data are produced in a coherent form that can be easily read. A final report is produced, eliminating typing time and errors.

## INTRODUCTION

The Environmental Monitoring Section of the Oak Ridge Y-12 Plant\* Radiation Safety Department has the responsibility of monitoring particulate emissions around the Y-12 Plant. Eleven monitoring stations have been placed around the perimeter of the plant. The filters in each system are changed on a weekly basis and are sent to the Plant Laboratory for gross alpha/beta counting. The weekly filters from each site are composited and analyzed quarterly for  $^{238}\text{U}$ ,  $^{235}\text{U}$ , and  $^{234}\text{U}$  by alpha spectroscopy. In order to arrive at quarterly concentration values reported in microcuries per cubic centimeter of air, several calculations are involved. A FORTRAN program (AIRFIL) has been written which manages all the raw input data, calculates the final concentrations and prints both raw data and final report in a matter of minutes.

This report describes the analysis and the FORTRAN program used in this procedure. Copies of the procedure and the program are included in Appendices A and B, respectively.

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\* Operated for the U.S. Department of Energy by the Union Carbide Corporation.

PROCEDUREGross Alpha/Beta Counting 2

The filter halves are counted for five minutes on a Sharp alpha/beta proportional counter with an alpha efficiency of 30% and a beta efficiency of 45%. The fact that the samples are collected on paper filters affects counting efficiency, therefore absorption factors (paper factors) are applied to the instrumental efficiencies. Paper factors for this particular filter paper (Whatman 41) have been determined to be 0.73 for beta and 0.51 for alpha counting.

Sample Preparation for Isotopic Uranium Alpha Counting 2

The samples are prepared for isotopic alpha counting using the procedure found in Appendix A of this report.

Isotopic Uranium Alpha Counting

An alpha spectrometer equipped with 600 mm<sup>2</sup> silicon surface barrier detectors and a multichannel analyzer is used. The detectors have an alpha efficiency of 10-15% in the configuration used. The efficiency is determined by using an in-house standard containing <sup>238</sup>U, <sup>235</sup>U and <sup>234</sup>U. Regions of interest for the isotopes are also determined with this standard. After the instrument has been calibrated, each sample is counted 60 minutes. <sup>232</sup>U counts are used to calculate a recovery factor which is applied to each isotopic count (H. A. T. M., 1984)

*[Handwritten notes and scribbles follow]*



# FORTRAN PROGRAM

A FORTRAN program called AIRFIL has been written to perform all data manipulations and calculations. The following discussion describes AIRFIL and the equations it uses.

All data for AIRFIL are entered via the keyboard in response to appropriate prompts. The year and quarter during which the samples were collected are stored to identify the sample set on the final report heading. Next, a series of background data is requested, which includes the counting time in minutes and the number of days over which the samples were counted. Although as many as three detectors can be used, the analyses require a few days, making it necessary to enter the day number to correctly identify the daily variant information.

Planchet blank values are an indication of the baseline status of the detectors under conditions which closely simulate the counting of the samples. These values are determined each morning and vary slightly from day to day and from detector to detector. There is a planchet blank value for each of the four uranium isotopes of interest for each detector each day over which the samples were counted. These values are requested by the program.

Next, values for uranium standards containing  $^{238}\text{U}$ ,  $^{235}\text{U}$  and  $^{234}\text{U}$  are requested. Like planchet blanks, the standards are counted in each detector each day of counting. Also requested are the total disintegrations per minute (dpm) contained on each standard.

Using the above data, the first calculations performed by the program are the detector efficiencies. An efficiency is determined for each detector on each counting day. In the calculation, the appropriate planchet blank is subtracted from each isotopic standard value. The equation is

$$E(n,d)=[SV(i,n,d)-PB(i,n,d)]/T/G(n,d) \quad (1)$$

where:

$E(n,d)$ =Efficiency of detector  $n$  on day  $d$   
 $SV(i,n,d)$ =Standard count value of isotope  $i$  in detector  $n$   
on day  $d$ ,  
 $PB(i,n,d)$ =Planchet blank value of isotope  $i$  in detector  $n$   
on day  $d$ ,  
 $T$ =Counting time in minutes, and  
 $G(n,d)$ =Total dpm of  $^{238}\text{U}$ ,  $^{235}\text{U}$  and  $^{234}\text{U}$  on planchet in  
detector  $n$  on day  $d$

All samples are spiked with a small amount (10-15 dpm) of  $^{232}\text{U}$  as an internal standard. Normally, the spike contains traces of  $^{238}\text{U}$ ,  $^{235}\text{U}$ , and  $^{234}\text{U}$  along with the  $^{232}\text{U}$ . These additional counts are of course added to the samples along with the internal standard. To compensate for this and to monitor sample contamination throughout the procedure, three sample blanks are spiked and carried through the procedure along with the samples. The blanks consist of the same type filter paper (Whatman 41) and the same number of filters as the samples.

A gross alpha/beta count is made on each filter half. The filters are held a minimum of three days before they are counted to allow possible thorium daughters to decay. Once counted, the filters from each site are retained until the end of the quarter so that isotopic uranium alpha determinations can be made on each site composite. The raw alpha/beta counts are converted to dpm using the following equations:

$$\text{Alpha Dpm} = 2[\text{ACNTS} - \text{ABKG} / \text{T} / 0.51 / \text{AEFF}] \quad (4)$$

where:

ACNTS=Alpha counts,  
ABKG=Instrument alpha background counts,  
T=Counting time in minutes,  
AEFF=Detector alpha efficiency,  
2=Factor to convert dpm per half filter to dpm per total filter, and  
0.51=Alpha paper factor.

And

$$\text{Beta Dpm} = 2[\text{BCNTS} - \text{BBKG} / \text{T} / 0.73 / \text{BEFF}] \quad (5)$$

where:

BCNTS=Beta counts,  
BBKG=Instrument beta background counts,  
T=Counting time in minutes,  
BEFF=Detector beta efficiency,  
2=Factor to convert dpm per half filter to dpm per total filter, and  
0.73=Beta paper factor.

The alpha/beta dpm for each site are summed to obtain total gross alpha/beta dpm per site per quarter. The dpm are then converted to microcuries for final output.

The beginning and ending air flows from each site and the number of days between installation and removal of the filters are used in the following equation to calculate the volume of air in cubic meters pulled through each filter.

$$\text{FLO} = [\text{FLOW1} + \text{FLOW2}] / 2 [\text{DAYS}] [0.0283 \text{m}^3 / \text{ft}^3] [1440 \text{min} / \text{day}] \quad (6)$$

where,

FLO=Total flow in cubic meters  
FLOW1=Initial flow in cfm  
FLOW2=Final flow in cfm, and  
Days=Number of days in sampling period.

The weekly volumes are summed to arrive at the total cubic meters of air collected at a site during the quarter. The cubic meters are then converted to cubic centimeters to accommodate the requested output. The total gross alpha/beta concentrations are reported as microcuries per cubic centimeter.

Counts for the three uranium isotopes of interest and the  $^{232}\text{U}$  internal standard are entered along with the detector number and the counting day number on which the composite was counted. A sample recovery value is calculated as in Equation (2). Again, if the recovery exceeds one, the value is written to the terminal to inform the analyst that a potential problem may exist and that the recovery has been set to 1.000 for the remainder of the calculation.

The sample counts for each isotope are then converted to dpm as in Equation (3). Once this is completed, the program subtracts the appropriate average sample blank dpm from each isotope. This cycle is repeated until the data from each site is entered.

Detection limits are calculated for each isotope and for the gross alpha/beta values. By convention, the detection limits are calculated as twice the value of the square root of the background levels. However, there are details which need to be amplified. The determination of the isotopic detection limits begins with the conversion of the sample blank counts to dpm, with no planchet blank subtraction. The values for a given isotope from each of the sample blanks are then averaged. This produces three background values, one for each isotope of interest. As in the samples, the number of dpm for each isotope is doubled to represent a total filter. The square roots of these numbers are then multiplied by 2 and divided by the average air volume per site, followed by conversion to microcuries per cubic centimeter.

The gross alpha/beta detection limits are determined by averaging the alpha and beta detector backgrounds. Unlike the isotopic limits, the averaged values are not doubled since they reflect only empty counter backgrounds and not filters. Two times the square roots of these averages are divided by the average air volume per site.

AIRFIL produces a disk file which contains a summary of the preliminary data as entered by the analyst and several intermediate results. Two copies of a final report follow, which list the isotopic and gross alpha/beta values in microcuries per cubic centimeter. Detection limits are listed at the end of each data column. A brief summary of the major equations used in AIRFIL is presented. A line is provided for a signature which verifies that the report has been reviewed and approved.

This program works well and has fulfilled its goals of reduced calculation time, orderly data manipulation and management, reduced errors due to redundant calculations and eliminated typing turnaround time. However, the program is not perfect since it requires considerable keyboard data entry. Future work will be directed to on-line data acquisition for as much data as possible.

## APPENDIX A

RADIOCHEMICAL METHOD FOR DETERMINING URANIUM  
IN AIR FILTERS1. Scope and Application

This method is applicable to the determination of the isotopes of uranium in paper and Hollingsworth types of air filters.

2. Summary of Method

2.1  $^{232}\text{U}$  tracer is added to the dissolved filter solution and equilibrated with the uranium in the sample. Plutonium and thorium are separated by adsorption on anion exchange resin under conditions that allow uranium to remain in the effluent. Repeated liquid-liquid extractions with methyl isobutyl ketone (hexone) are used to purify the uranium. The final hexone extract is dried on a stainless steel plate, and the determination of the uranium isotopes is made by alpha spectrometric measurements using a silicon surface-barrier detector to count the plate.

2.2 The lowest concentration reported is 0.04 pCi/total. Typically for filters that have filtered  $1 \times 10^3 \text{ m}^3$  of air, the lowest concentration reported then is  $4 \times 10^{-5} \text{ pCi/m}^3$ .

3. Sample Handling and Preservation

Filters should be handled as little as possible to avoid loss of particulates and should be stored in plastic containers such as polyethylene bags..

4. Interferences

4.1 Iron in concentrations of milligrams per gram of sample tends to follow uranium throughout the chemistry and causes serious degradation of alpha measurements.

4.2  $^{234}\text{U}$  cannot be distinguished easily from  $^{233}\text{U}$ .

## 5. Apparatus

- 5.1 Analytical balance
- 5.2 Muffle furnace
- 5.3 Hot plate
- 5.4 Centrifuge
- 5.5 Vortex mixer
- 5.6 Extraction vials, 50-mL with plastic-lined screw caps
- 5.7 Teflon beakers, 250-mL size
- 5.8 Transfer pipettes
- 5.9 Lab glassware
  - 5.9.1 Beakers, 100-, 250-, and 600-mL
  - 5.9.2 Centrifuge tubes, 50-mL glass
  - 5.9.3 Glass ion-exchange column, 0.8 cm ID by 25 cm long, fitted with a stopcock and reservoir
- 5.10 Stainless steel disks
- 5.11 Multichannel analyzer system with silicon surface-barrier detector(s)

## 6. Reagents

- 6.1 Nitric acid ( $\text{HNO}_3$ ), concentrated
- 6.2 Nitric acid ( $\text{HNO}_3$ ), 8M: Add 500 ml of concd  $\text{HNO}_3$  to 500 mL of water.
- 6.3 Aluminum nitrate solution [ $\text{Al}(\text{NO}_3)_3$ ], 2.8M: Dissolve 1050 grams of aluminum nitrate nonahydrate [ $\text{Al}(\text{NO}_3)_3 \times 9\text{H}_2\text{O}$ ] in a minimum of water with heat. Cautiously add 100 mL of concd ammonium hydroxide ( $\text{NH}_4\text{OH}$ ) with stirring until all of the precipitate dissolves; dilute to 1 liter with water.
- 6.4 Sodium nitrite ( $\text{NaNO}_2$ ), crystals
- 6.5 Methyl isobutyl ketone (hexone)
- 6.6 Potassium bromate ( $\text{KBrO}_3$ ), crystals

6.7  $^{232}\text{U}$ uranium tracer solution: Dilute a stock solution  $^{232}\text{U}$ uranium to a concentration of 10 dis/min/mL.

6.8 Anion exchange resin: Dowex 1 x 4 (50-100 mesh, chloride form) or equivalent.

6.9 Hydrogen peroxide ( $\text{H}_2\text{O}_2$ ), 30% solution

6.10 Hydrofluoric acid (HF), concentrated

## 7. Procedure

7.1 Weigh an aliquot of the filter(s) and place in an adequately sized beaker. Relate weight to total sample to determine air-flow volume.

7.2 Place the beaker and sample in a muffle furnace and set the temperature to 210°C.

7.3 Carbonize the sample by allowing it to remain at 210°C for 8 h.

7.4 Raise the temperature of the furnace to 375°C and allow the sample to ash at this temperature for 16 h; finally ash at 525°C for 24 h.

7.5 Transfer the ashed sample to a 250-mL Teflon beaker.

7.6 Add 25 mL of concd  $\text{HNO}_3$  and 25 mL of concd HF.  
NOTE - Paper filters may be completely soluble in  $\text{HNO}_3$ ; therefore, the addition of HF may be excluded, and the procedure can be continued at step 7.14.

7.7 Place the sample on a hot plate and take to dryness.

7.8 Repeat steps 7.6 and 7.7 twice.

7.9 Add 15 mL of concd  $\text{HNO}_3$  and take to dryness.

7.10 Repeat step 7.9 twice.

7.11 Take up the residue in 25 mL of 8M  $\text{HNO}_3$  and 3 to 5 mL of  $\text{H}_2\text{O}$ .

7.12 Transfer the sample to the original ashing beaker.

7.13 Place the beaker on a hot plate and digest with the addition of 30%  $\text{H}_2\text{O}$  in 1-mL portions until the solution is clear.

7.14 Add 1.00 mL of 10 dis/min/mL  $^{232}\text{U}$ uranium tracer solution.

- 7.15 Adjust the acidity to 8M  $\text{HNO}_3$ .
- 7.16 Add 250 mg of  $\text{NaNO}_2$  crystals; place on hot plate; bring to a boil rapidly; immediately remove from heat and allow the sample to digest for 20 min.
- 7.17 While the sample is digesting, prepare a resin column as follows.
  - 7.17.1 Place a glass-wool plug in the bottom of the column described in step 5.9.3.
  - 7.17.2 Slurry the resin (see step 6.8) with water and immediately discard the fines by decanting. Repeat as necessary until fines are removed.
  - 7.17.3 Transfer 4 mL of resin to the column with water. Prevent any channeling by maintaining the solution level above the resin by use of the stopcock.
  - 7.17.4 Place a glass-wool plug on top of the resin.
  - 7.17.5 Convert the resin to the nitrate form by passing several column volumes of 8M  $\text{HNO}_3$  through the column until the resin is free of chloride ions.
- 7.18 Transfer the sample solution, which should be at room temperature, to the prepared resin column.
- 7.19 Place a 250-mL beaker beneath the column and allow the sample solution to drain into the beaker at a flow rate of 2 mL/min.
- 7.20 Rinse the beaker with 25 mL of 8M  $\text{HNO}_3$  and transfer the rinse to the column.
- 7.21 Allow the rinse to drain into the beaker also.
- 7.22 Place the beaker containing the column effluent on a hot plate and take to dryness.
- 7.23 Dissolve the residue in 10 mL of  $\text{Al}(\text{NO}_3)_3$  solution and transfer to an extraction vial using a minimum of  $\text{Al}(\text{NO}_3)_3$  to rinse the beaker.
- 7.24 Add an equal volume of hexone and extract on a Vortex mixer for 10 min.
- 7.25 Centrifuge for 2 min to separate the phases and discard the aqueous phase.
- 7.26 Add an equal volume of water and back-extract into the water on Vortex mixer for 10 min.

- 7.27 Centrifuge for 2 min. to separate the phases.
- 7.28 Transfer the aqueous phase to a 100-mL beaker.
- 7.29 Repeat steps 7.26, 7.27, and 7.28.
- 7.30 Place the beaker containing the water strip solution on a hot plate and take to dryness.
- 7.31 Add enough 8M  $\text{HNO}_3$  to moisten the residue.
- 7.32 Add 10 to 20 mg of  $\text{KBrO}_3$  crystals and digest for 10 min.
- 7.33 Dissolve and transfer the residue to an extraction vial with 5 mL of  $\text{Al}(\text{NO}_3)_3$  solution.
- 7.34 Repeat step 7.24 using 1 mL of hexone; repeat step 7.25.
- 7.35 Transfer the entire hexone extract by drops to a stainless steel disk placed on a hot plate set at  $100^\circ\text{C}$ .
- 7.36 Flame the disk to a red heat.
- 7.37 Measure the uranium alpha activities by pulsing with a silicon surface-barrier detector and multichannel analyzer.



```

C*****
C
C      AIR FILTER CALCULATION PROGRAM
C
C      APRIL 1983      RL HOWELL
C
C*****
C      THIS PROGRAM CALCULATES THE CONCENTRATION OF U238, U235, AND
C      U234 IN AIR FILTERS SAMPLING THE Y-12 AREA. DATA INCLUDING
C      COUNTER BLANK COUNTS, STANDARDS, FLOW DATA, AND GROSS ALPHA
C      AND BETA COUNTS ARE ENTERED. A REPORT FILE, AIRRPT.DAT, IS
C      GENERATED WHICH CONTAINS INTERMEDIATE DATA AND A FINAL
C      REPORT. THE PROGRAM CAN HANDLE UP TO 22 SAMPLING SITES, 20
C      FILTERS PER SITE, 3 DETECTORS, AND 5 COUNTING DAYS. THE
C      DETECTION LIMITS ARE CALCULATED AS 2 * SQRT (BACKGROUND).
C      ALL FILTER RESULTS ARE MULTIPLIED BY 2 TO ACCOUNT FOR THE
C      TOTAL FILTER.
C
C      DIMENSION ISOTPE(4), PLN(4,3,5), STD(3,3,5), ISAM(3)
C      DIMENSION FLO1(22,20), FLO2(22,20), A(22,20), B(22,20), ALP(22)
C      DIMENSION BET(22), DCTR(3), GROSS(3,5), BLK(4,3), ABKG(20)
C      DIMENSION COUNTS(4,22), DAYS(22), IDET(22), IDAY(5)
C      DIMENSION BLKAVG(3), SUMFLO(22), BLKCNT(4,3), DPMS(4,22)
C      DIMENSION BEFF(20), ACNTS(22,20), BCNTS(22,20), DPMFIL(3,22)
C      DIMENSION DPMLIM(3), BLKLIM(3,3), BBKG(20), AEFF(20)
C      DIMENSION ALPFIL(22), BETFIL(22)
C
C      ! DATA INITIALIZATION !
C
C      DATA ISOTPE(1)/238/, ISOTPE(2)/235/, ISOTPE(3)/234/
C      DATA ISOTPE(4)/232/, DCTR(1)/'A'/, DCTR(2)/'B'/, DCTR(3)/'C'/
C      DATA ISAM(1)/1/, ISAM(2)/2/, ISAM(3)/3/
C
C      INTEGER*2      DETNUM, DAYNUM
C      REAL*4  TIME,EFF(3,5),INTSTD
C
C      ENTER YEAR AND QUARTER FOR REPORT
C
C      WRITE (5,8)
C      8      FORMAT(1X,18X,'*** AIR FILTER CALCULATION PROGRAM ***',///,
C      1      1X,'ENTER YEAR IN WHICH SAMPLES WERE COLLECTED '
C      2      '(4 DIGITS): ', $)
C      READ (5,2) IYEAR
C      2      FORMAT (I4)
C      WRITE (5,3)
C      3      FORMAT (1X,'ENTER QUARTER: ', $)
C      READ (5,4) IQTR
C      4      FORMAT (I1)
C
C      ENTER COUNTING PARAMETERS
C

```

```

WRITE(5,5)
5  FORMAT(1X,'ENTER COUNTING TIME IN MINUTES: ', $)
   READ (5,6) TIME
6  FORMAT (F3.0)
   WRITE (5,10)
10  FORMAT (1X,'ENTER NUMBER OF DAYS OVER WHICH',
1    ' SAMPLES WERE COUNTED: ', $)
   READ (5,11) NDAYS
11  FORMAT (I1)
C
C
C  ENTER PLANCHET BLANKS
C
DO 26 J=1,NDAYS
12  DO 25 I=1,3      ! DETECTORS !
   DO 23 N=1,4      ! ISOTOPES !
   WRITE (5,15) ISOTPE(N), DCTR(I), J
15  FORMAT(1X,'ENTER U',I3,' PLANCHET BLANK FOR DETECTOR ',1A,
1    ' ON DAY NUMBER ',I1,' : ', $)
   READ (5,20) PLN(N,I,J)
20  FORMAT(F3.0)
23  CONTINUE
25  CONTINUE
26  CONTINUE
C
C
C  ENTER STANDARD COUNTS
C
DO 42 J=1,NDAYS
DO 40 I=1,3
DO 38 N=1,3
WRITE (5,30) ISOTPE(N), DCTR(I), J
30  FORMAT(1X,'ENTER U',I3,' STANDARD COUNT FOR DETECTOR ',1A,
1    ' ON DAY NUMBER ',I1,' : ', $)
   READ(5,35) STD(N,I,J)
35  FORMAT(F3.0)
38  CONTINUE
40  CONTINUE
42  CONTINUE
C
C
C  ENTER GROSS DPM
C
DO 55 J=1,NDAYS
DO 54 I=1,3
WRITE (5,43) DCTR(I), J
43  FORMAT(1X,'ENTER GROSS DPM FOR DETECTOR ',1A,' ON DAY NUMBER ',
1    I1,' : ', $)
   READ (5,50) GROSS(I,J)
50  FORMAT(F5.0)
54  CONTINUE
55  CONTINUE

```

```

C
C
C
C
C ! CALCULATE EFFICIENCY !
C
      TEMP = 0
      DO 70 J=1,NDAYS
      DO 63 N=1,3 ! DETECTOR NUMBER !
      DO 62 I=1,3 ! ISOTOPE !
      TMP1=STD(I,N,J) - PLN(I,N,J)
      TEMP = TEMP + TMP1
62      CONTINUE
      EFF(N,J) = TEMP / TIME / GROSS(N,J)
      TEMP = 0
63      CONTINUE
70      CONTINUE
C
C      ENTER SPIKE DPM

      WRITE (5,64)
64      FORMAT (1X,'ENTER THE SPIKE DPM: ', '$)
      READ (5,80) SPK
80      FORMAT(F3.0)
C
C
C      ENTER SAMPLE BLANK DATA
C
      DO 75 I=1,3 !SAMPLE BLANK NUMBER!
      WRITE (5,65) I
65      FORMAT(1X,'ENTER DETECTOR NUMBER FOR SAMPLE BLANK ',I1,': ', '$)
      READ (5,66) DETNUM
66      FORMAT(I1)
      WRITE (5,56) I
56      FORMAT (1X,'ENTER THE DAY NUMBER FOR SAMPLE BLANK ',I1,': ', '$)
      READ (5,57) DAYNUM
57      FORMAT (I1)
C
      DO 74 N=1,3
      WRITE(5,69) ISOTPE(N), I
69      FORMAT(1X,'ENTER U',I3,' COUNTS FOR SAMPLE BLANK ',I1,': ', '$)
      READ (5,71) BLKCNT(N,I)
71      FORMAT(F3.0)
C
74      CONTINUE
      WRITE (5,45) I
45      FORMAT (1X,'ENTER U232 COUNTS FOR SAMPLE BLANK ',I1,': ', '$)
      READ (5,46) INTSTD
46      FORMAT (F3.0)
C      SUBTRACT PLANCHET BLANK FROM THE INTERNAL STANDARD
      INTSTD = INTSTD - PLN(4, DETNUM, DAYNUM)

```

```

C      CALC RECOVERY FOR SAMPLE BLANKS
      BLKREC = INTSTD / TIME / EFF(DETNUM, DAYNUM) / SPK
      IF (BLKREC .LT. 1.) GOTO 351
      WRITE (5,350) I, BLKREC
350    FORMAT (1X, 'THE RECOVERY VALUE FOR SAMPLE BLANK ',
1      I1, ' WAS ', F7.4, '. IT HAS BEEN RESET TO 1.000')
      BLKREC = 1.
351    CONTINUE
C
C      CONVERT SAM BLK CNTS TO DPM
C
      DO 49 N=1,3      !ISOTOPES!
      BLK(N,I) = (BLKCNT(N,I) - PLN(N,DETNUM,DAYNUM)) / TIME
1      / EFF(DETNUM, DAYNUM) / BLKREC
      BLKLIM(N,I)=BLKCNT(N,I) / TIME / EFF(DETNUM,DAYNUM) / BLKREC
49    CONTINUE
75    CONTINUE
C
C      AVERAGE THE ISOTOPES IN THE SAM BLKS AND CALC DETECTION LIMITS
C
      TMP4 = 0
      TMP2 = 0
      DO 78 N=1,3      !ISOTOPE!
      DO 77 I=1,3      !SAMPLE!
      TMP1 = BLK(N,I)
      TMP2 = TMP2 + TMP1
      TMP3 = BLKLIM(N,I)
      TMP4 = TMP4 + TMP3
77    CONTINUE
      BLKAVG(N) = TMP2 / 3.
      DPMLIM(N) = TMP4 / 3.
      DPMLIM(N) = 2. *.SQRT(2. * DPMLIM(N))
      TMP2 = 0
78    CONTINUE
C
C      NOW ENTER SAMPLE DATA
C
      WRITE(5,81)
81    FORMAT(1X, 'ENTER NUMBER OF SAMPLE SITES: ', $)
      READ (5,82) NSITES
82    FORMAT(I2)
C
C
      WRITE (5,85)
85    FORMAT(1X, 'ENTER NUMBER OF FILTERS COMPOSITED FROM EACH SITE: ', $)
      READ (5,86) NFILTR
86    FORMAT(I2)
      ALPBKG = 0
      BETBKG = 0
      DO 110 N = 1,NFILTR

```

```

C
DO 90 I=1,NSITES
WRITE (5,88) I,N
88  FORMAT(1X,'ENTER FLOW 1 FOR SITE ',I2,' FILTER ',I2,': ',,$)
   READ (5,89) FLO1(I,N)
89    FORMAT(F3.1)
90    CONTINUE
   DO 92 I = 1, NSITES
   WRITE (5,91) I,N
91    FORMAT (1X,'ENTER FLOW 2 FOR SITE ',I2,' FILTER ',I2,': ',,$)
   READ (5,89) FLO2(I,N)
92    CONTINUE
C
   WRITE (5,93)
93    FORMAT(1X,6X,'NUMBER OF DAYS = ',,$)
   READ (5,94) DAYS(N)
94    FORMAT(F2.0)
   WRITE (5,95) N
95    FORMAT (1X,'ENTER ALPHA BACKGROUND FOR FILTER ',I2,': ',,$)
   READ (5,97) ABKG(N)
   WRITE (5,96) N
96    FORMAT (1X,'ENTER BETA BACKGROUND FOR FILTER ',I2,': ',,$)
   READ (5,97) BBKG(N)
97    FORMAT (F3.0)
   WRITE (5,98)
98    FORMAT (1X,'ENTER ALPHA METAL EFFICIENCY: ',,$)
   READ (5,100) AEFF(N)
   WRITE (5,99)
99    FORMAT (1X,'ENTER BETA METAL EFFICIENCY: ',,$)
   READ (5,100) BEFF(N)
100   FORMAT (F4.2)
   WRITE (5,101)
101   FORMAT (1X,'ENTER ALPHA/BETA COUNTING TIME: ',,$)
   READ (5,102) CTIME
102   FORMAT (F2.0)
   DO 105 I = 1, NSITES
   WRITE (5,103) I, N
103   FORMAT (1X,'ENTER ALPHA COUNTS FOR SITE ',I2,' FILTER ',I2,': ',,$)
   READ (5,104) ACNTS(I,N)
104   FORMAT (F6.0)
C
C   CONVERT COUNTS TO DPM

   A(I,N) = 2. * (ACNTS(I,N) - ABKG(N))/(CTIME * 0.51 * AEFF(N))
105   CONTINUE
   AABKG = ABKG(N) / (CTIME * 0.51 * AEFF(N))
   DO 107 I = 1, NSITES
   WRITE (5,106) I, N
106   FORMAT(1X,'ENTER BETA COUNTS FOR SITE ',I2,' FILTER ',I2,': ',,$)
   READ (5,104) BCNTS(I,N)
C
C   CONVERT COUNTS TO DPM

```

```

107      B(I,N) = 2. * (BCNTS(I,N) - BBKG(N)) / (CTIME * 0.73 * BEFF(N))
      CONTINUE
      BBBKG = BBKG(N) / (CTIME * 0.73 * BEFF(N))
C
C      SUM ALP AND BETA BKGS TO AVERAGE LATER
C
      ALPBKG = ALPBKG + AABKG
      BETBKG = BETBKG + BBBKG
110     CONTINUE
C
C      SUM ALP AND BETA DPMS AT EACH SITE
C
      DO 112 I=1,NSITES
      DO 111 N=1,NFILTR
      TMP1 = A(I,N)
      TMP2 = B(I,N)
      ALP(I) = ALP(I) + TMP1
      BET(I) = BET(I) + TMP2
111     CONTINUE
112     CONTINUE
C
C      NOW AVERAGE ALP AND BETA BACKGROUNDS
C
      FILTRS = NFILTR
      ALPBKG = ALPBKG / FILTRS
      BETBKG = BETBKG / FILTRS
C
C      ! CHANGE FLOW DATA IF MISTAKES WERE ENTERED !
C
113     WRITE (5,114)
114     FORMAT (1X,10X,'0 -- FLOW DATA ENTERED CORRECTLY',/
1       1X,10X,'1 -- FLOW DATA NEEDS CORRECTION',/
2       1X,10X,'      ENTER SELECTION: ',)$)
      READ (5,115) IEDIT
115     FORMAT (I1)
      IF (IEDIT .EQ. 0) GO TO 124
      WRITE (5,116)
116     FORMAT (1X,'ENTER FILTER NUMBER: ',)$)
      READ (5,117) IFIL
117     FORMAT (I2)
      WRITE (5,118)
118     FORMAT (1X,'ENTER SITE NUMBER: ',)$)
      READ (5,119) ISIT
119     FORMAT (I2)
      WRITE (5,120)
120     FORMAT (1X,'ENTER FLOW 1: ',)$)
      READ (5,121) ANS
121     FORMAT (F3.1)
      FLO1(ISIT, IFIL) = ANS
      WRITE (5,122)

```

```

122  FORMAT (1X,'ENTER FLOW 2: ',,$)
      READ (5,121) ANS
      FLO2(ISIT,IFIL) = ANS
      WRITE (5,123)
123  FORMAT (1X,'THE CHANGE HAS BEEN MADE.')
      GO TO 113

C
C  !NOW ENTER ISOTOPIC DATA !
C
C
124  DO 155 I=1,NSITES
      WRITE (5,125)
125  FORMAT(1X,///,1X,18X,'*** DATA ENTRY ***',//)
      WRITE (5,126) I
126  FORMAT(1X,'FOR SITE NUMBER ',I2,': ')
      WRITE (5,127)
127  FORMAT(1X,6X,'ENTER DETECTOR NUMBER: ',,$)
      READ (5,128) IDET(I)
128  FORMAT (I1)
      DETNUM = IDET(I)

C
      WRITE (5,129)
129  FORMAT (1X,6X,'ENTER DAY NUMBER: ',,$)
      READ (5,132) DAYNUM
132  FORMAT (I1)
      IDAY(I) = DAYNUM

C
C
      DO 140 N=1,4      !ISOTOPES!
      WRITE (5,130) ISOTPE(N)
130  FORMAT(1X,6X,'U',I3,' COUNTS: ',,$)
      READ (5,131) COUNTS(N,I)
131  FORMAT(F6.0)
140  CONTINUE

C
C  CALCULATE RECOVERY
C
      RCV=(COUNTS(4,I)-PLN(4,DETNUM,DAYNUM))/TIME/EFF (DETNUM,DAYNUM)/SPK
      IF (RCV .LT. 1.) GOTO 145
      WRITE (5,141) I, RCV
141  FORMAT(1X,'THE RECOVERY FOR SITE ',I2,' SAMPLES WAS',
1      F7.4,'.',/,1X,'IT HAS BEEN RESET TO 1.000')
      RCV = 1.
145  CONTINUE

C
C  CONVERT COUNTS TO DPM
C
      DO 150 N=1,3      ! ISOTOPES !
      DPMS(N,I)=(COUNTS(N,I)-PLN(N,DETNUM,DAYNUM)) / TIME
1      / EFF (DETNUM,DAYNUM) / RCV
      DPMS(N,I) = DPMS(N,I) - BLKAVG(N)
      IF (DPMS(N,I) .LT. 0) DPMS(N,I) = 0
150  CONTINUE

```

```

155     CONTINUE
C
C
C
C     !CALCULATE CUBIC METERS OF AIR!
C
      SITENO = NSITES
      TOTFLO = 0
      DO 178 I=1,NSITES
      SUMFLO(I) = 0
178     CONTINUE
      DO 185 I=1,NSITES
      DO 180 N=1,NFILTR
      TFLO = ((FLO1(I,M)+FLO2(I,N))/2) * 40.752 * DAYS(N)
      SUMFLO(I) = SUMFLO(I) + TFLO
180     CONTINUE
      TOTFLO = TOTFLO + SUMFLO(I)
185     CONTINUE
      AVGFLO = TOTFLO / SITENO
      DO 188 N=1,3     !ISOTOPES!
      DPMLIM(N) = DPMLIM(N) / AVGFLO / 2.22E12
188     CONTINUE
C
C
C     !CALCULATE MICROCURIES PER CUBIC CENTIMETER!
C
      DO 190 I=1, NSITES
      DO 189 N=1, 3
      DPMFIL(N,I) = DPMS(N,I) * 2
      DPMS(N,I) = DPMS(N,I) * 2. / SUMFLO(I) / 2.22E12
189     CONTINUE
      ALPFIL(I) = ALP(I)
      BETFIL(I) = BET(I)
      ALP(I) = ALP(I) / SUMFLO(I) / 2.22E12
      BET(I) = BET(I) / SUMFLO(I) / 2.22E12
190     CONTINUE
      ALPBKG = 2. * SQRT(ALPBKG) / AVGFLO / 2.22E12
      BETBKG = 2. * SQRT(BETBKG) / AVGFLO / 2.22E12
C
      OPEN (UNIT=2, NAME='AIRFIL.RPT', TYPE='NEW',
1       FORM='FORMATTED', ACCESS='SEQUENTIAL',
2       CARRIAGE CONTROL ='FORTRAN')
C     !OUTPUT!
C
      WRITE (2,200)
200     FORMAT(1X, 55X, 'AIR FILTER COMPOSITES REPORT',//,
1       1X, 63X, 'DATA LISTING',/////))
C
C
C
      WRITE (2,210)

```



```

210  FORMAT(1X,56X,'----- SAMPLE BLANKS -----',//,
      1    1X,45X,'ONE',19X,'TWO',18X,'THREE',/,
      1    1X,38X, 3('COUNTS',6X,'DPM',7X),//)
C
C
C
      WRITE(2,220) (ISOTPE(J), (BLKCNT(J,I), BLK(J,I), I=1,3), J=1,3)
220  FORMAT(1X,20X,'U',I3,14X, 3(F5.0,5X,F5.0,7X),/,1X,20X,'U',
      1    I3,14X, 3(F5.0,5X,F5.0,7X),/,1X,20X,'U',I3,14X
      1    3(F5.0,5X,F5.0,7X),///)
C
C
      ! DETECTOR DATA OUTPUT !
      DO 262 K=1,NDAYS
      WRITE (2,240) K

240  FORMAT (1X,56X,'----- DETECTOR DATA -----',/,1X,66X,
      1    'DAY 'I1,/,1X,44X,
      2    'ONE', 19X, 'TWO', 18X, 'THREE',//)
      WRITE (2,245) (ISOTPE(J), (PLN(J,I,K), I=1,3), J=1,3)
245  FORMAT (1X,'PLANCHET BLANKS',5X,'U',I3,1X,3(17X,F5.0),
      1    /,1X,20X,'U',I3,1X, 3(17X,F5.0),/,1X,20X,'U',I3,
      2    1X, 3(27X,F5.0),//)
      WRITE (2,250) (ISOTPE(J), (STD(J,I,K), I=1,3), J=1,3)
250  FORMAT (1X,'STANDARD COUNTS',5X,'U',I3,1X,3(17X,F5.0)
      1    /,1X,20X,'U',I3,1X,3(17X,F5.0),/,1X,20X,'U',I3,1X,3(17X,F5.0))
      WRITE (2,255) (GROSS(I,K), I=1,3)
255  FORMAT (1X,3X,'GROSS DPM',13X,3(17X,F5.0))
      WRITE (2,260) (EFF(I,K), I=1,3)
260  FORMAT (1X,3X,'EFFICIENCY',14X,3(17X,F5.4),///)
262  CONTINUE
      WRITE (2,360)
360  FORMAT (1X,54X,'----- ALPHA / BETA DATA -----',/,1X,40X,
      1    'BACKGROUND COUNTS',23X,'METAL EFFICIENCY',/,1X,36X,
      2    'ALPHA',15X,'BETA',16X,'ALPHA',14X,'BETA',//)
      WRITE (2,361) (N,ABKG(N),BBKG(N),AEFF(N), BEFF(N), N=1,NFILTRS)
361  FORMAT (1X,20X, 'FILTER ',I2,8X,F3.0,16X,F3.0,16X,F4.2,14X,F4.2)
      WRITE (2,265)
265  FORMAT (///,1X,56X,'----- AIR FLOW DATA -----',//)
      DO 285 I = 1, NSITES
      WRITE (2,270) I, SUMFLO(I)
270  FORMAT(1X,///,1X,60X 'SITE NUMBER ',I2,/,1X,51X,'TOTAL ',
      1    ' FLOW = ',F8.1,' CUBIC METERS',/,1X,35X,'FLOW 1',9X,
      2    'FLOW 2',10X,'DAYS',8X,'ALPHA CNTS',4X,'BETA CNTS',//)
      DO 280 J = 1, NFILTR
      WRITE (2,275) J,FLO1(I,J),FLO2(I,J),DAYS(J),ACNTS(I,J),
      1    BCNTS(I,J)
275  FORMAT(1X,20X,'SAMPLE ',I2,5X,F5.1,10X,F5.1,12X,F3.0,
      1    11X,F6.0,10X,F6.0)
280  CONTINUE
285  CONTINUE
      WRITE (2,287) (ISOTPE(N), N=1,4)

```

```

287  FORMAT(1X,///,1X,55X,'----- COUNTS ENTERED -----',//,
      1  1X,40X,3('U',I3,6X),'U',I3,4X,'DETECTOR',4X,'DAY',//)
      DO 289 N=1,NSITES
      WRITE (2,288) N,(COUNTS(I,N),I=1,4),IDET(N), IDAY(N)
288  FORMAT (1X,20X,'SITE NUMBER ',I2,6X,4(F5.0,5X),1X,I1,9X,I1)
289  CONTINUE
      WRITE (2,370)
370  FORMAT (///,1X,53X,'----- PRELIMINARY RESULTS -----',/,1X,47X,
      1  'DISINTEGRATIONS PER MINUTE PER TOTAL FILTER',//,1X,36X,
      2  'U238',11X,'U235',11X,'U234',11X,'ALPHA',10X,'BETA',//)
      DO 375 I = 1,NSITES
      WRITE (2,371) I, (DPMFIL(N,I),N=1,3), ALPFIL(I), BETFIL(I)
371  FORMAT (1X,20X,'FILTER ',I2,5X,5(1PE8.2, 7X))
375  CONTINUE
      DO 330 K = 1,2
      WRITE(2,290)
290  FORMAT('1',48X,41('*'),/,1X,48X,'*',39X,'*',/,1X,
      1  48X,'*',9X,'AIR FILTER COMPOSITES',9X,'*',/,1X,
      2  48X,'*',39X,'*',/,1X,48X,'*',13X,'FINAL REPORT',
      3  14X,'*',/,1X,48X,'*',39X,'*')
      GO TO (291,293,295,297), IQTR
291  WRITE (2,292) IYEAR
292  FORMAT (1X,48X,'*',10X,'FIRST QUARTER, ',I4,10X,'*',
      1  /,1X,48X,'*',39X,'*',/,1X,48X,41('*'),////)
      GO TO 299
293  WRITE (2,294) IYEAR
294  FORMAT (1X,48X,'*',10X,'SECOND QUARTER, ',I4,9X,'*',
      1  /,1X,48X,'*',39X,'*',/,1X,48X,41('*'),////)
      GO TO 299
295  WRITE (2,296) IYEAR
296  FORMAT (1X,48X,'*',10X,'THIRD QUARTER, ',I4,10X,'*',
      1  /,1X,48X,'*',39X,'*',/,1X,48X,41('*'),////)
      GO TO 299
297  WRITE (2,298) IYEAR
298  FORMAT (1X,48X,'*',10X,'FOURTH QUARTER, ',I4,9X,'*',
      1  /,1X,48X,'*',39X,'*',/,1X,48X,41('*'),////)
299  WRITE (2,322) (ISOTPE(N), N=1,3)
322  FORMAT(1X,5X,'SITE NUMBER',36X,'MICROCURIES PER CUBIC CENTIMETER',
      1  /,6X,11('-'),36X,32('-'),//,1X,10X,3(16X,'U',I3),12X,
      2  'GROSS ALPHA',10X,'GROSS BETA',/,1X,10X,3(16X,4('-')),
      3  12X,11('-'),10X,10('-'),//)
      DO 320 I=1,NSITES
      N = 1
      IF (DPMS(N,I) .LE. DPMLIM(N)) GO TO 302
      WRITE (2,300) I, DPMS(N,I)
300  FORMAT(1X,9X,I2,12X,1PE9.2, $)
      GO TO 304
302  WRITE (2,303) I, DPMLIM(N)
303  FORMAT (1X,9X,I2,12X, '<', 1PE8.2, $)
304  N = 2
      IF (DPMS(N,I) .LE. DPMLIM(N)) GO TO 306
      WRITE (2,305) DPMS(N,I)

```

```

305  FORMAT ('+', T13, 1PE9.2, $)
      GO TO 308
306  WRITE (2,307) DPMLIM(N)
307  FORMAT ('+', T13, '<', 1PE8.2, $)
308  N = 3
      IF (DPMS(N,I) .LE. DPMLIM(N)) GO TO 310
      WRITE (2,309) DPMS(N,I)
309  FORMAT ('+', T13, 1PE9.2, $)
      GO TO 312
310  WRITE (2,311) DPMLIM(N)
311  FORMAT ('+', T13, '<', 1PE8.2, $)
312  IF (ALP(I) .LE. ALPBKG) GO TO 314
      WRITE (2,313) ALP(I)
313  FORMAT ('+', T13, 1PE9.2, $)
      GO TO 316
314  WRITE (2,315) ALPBKG
315  FORMAT ('+', T13, '<', 1PE8.2, $)
316  IF (BET(I) .LE. BETBKG) GO TO 318
      WRITE (2,317) BET(I)
317  FORMAT ('+', T13, 1PE9.2, /)
      GO TO 320
318  WRITE (2,319) BETBKG
319  FORMAT ('+', T13, '<', 1PE8.2, /)
320  CONTINUE
      WRITE (2,325) (DPMLIM(N), N=1,3), ALPBKG, BETBKG
325  FORMAT (1X,/,1X,2X,'DETECTION LIMITS:',4X,5(1PE9.2,11X),/)
      WRITE (2,328)
328  FORMAT (1X,2X,'EQUATIONS USED IN THIS REPORT:',/,1X,7X,'DETECTION'
1    ' LIMIT = (2 * (BACKGROUND ** 0.5)) / AVG FLOW PER SITE',/,1X,
2    7X,'ISOTOPIC CONC. = (NET CNTS. / TIME / EFF / REC) - (NET'
3    ' SAM BLK CNTS. / TIME / EFF / REC)',/,1X,7X,'GROSS CONC. ='
6    'MIN / DAY * 10E6 CM**3 / M**3',/,1X,7X,'ALL VALUES WERE'
7    ' MULTIPLIED BY 2 TO ACCOUNT FOR THE TOTAL FILTER.',
8    '/',1X,7X,'THESE VALUES WERE CHECKED AND APPROVED BY',
9    20(' '),'.')
330  CONTINUE
      STOP
      END

```

C

# AIR FILTER COMPOSITES REPORT DATA LISTING

## ----- SAMPLE BLANKS -----

	COUNTS	ONE DPM	COUNTS	TWO DPM	COUNTS	THREE DPM
U238	0.	0.	2.	0.	2.	0.
U235	3.	0.	0.	0.	1.	0.
U234	17.	2.	18.	2.	6.	1.

## ----- DETECTOR DATA ----- DAY 1

		ONE	TWO	THREE
PLANCHET BLANKS	U238	1.	0.	2.
	U235	1.	1.	2.
	U234	11.	3.	11.
STANDARD COUNTS	U238	2.	2.	3.
	U235	124.	114.	116.
	U234	177.	181.	174.
GROSS DPM EFFICIENCY		35. .1381	36. .1356	32. .1448

----- DETECTOR DATA -----  
DAY 2

		ONE	TWO	THREE
PLANCHET BLANKS	U238	0.	2.	2.
	U235	2.	0.	1.
	U234	6.	2.	11.
STANDARD COUNTS	U238	24.	24.	29.
	U235	99.	119.	104.
	U234	165.	115.	157.
GROSS DPM EFFICIENCY		35. .1333	36. .1176	32. .1437

----- DETECTOR DATA -----  
DAY 3

		ONE	TWO	THREE
PLANCHET BLANKS	U238	0.	1.	0.
	U235	1.	1.	0.
	U234	1.	2.	0.
STANDARD COUNTS	U238	2.	8.	0.
	U235	115.	133.	0.
	U234	201.	180.	0.
GROSS DPM EFFICIENCY		35. .1505	35. .1510	1. .0000

## ----- ALPHA / BETA DATA -----

	BACKGROUND COUNTS		METAL EFFICIENCY	
	ALPHA	BETA	ALPHA	BETA
FILTER 1	10.	22.	0.33	0.49
FILTER 2	10.	22.	0.33	0.49
FILTER 3	10.	22.	0.33	0.49
FILTER 4	9.	22.	0.31	0.47
FILTER 5	9.	22.	0.31	0.47
FILTER 6	9.	22.	0.31	0.47
FILTER 7	9.	25.	0.31	0.48
FILTER 8	9.	25.	0.31	0.48
FILTER 9	10.	24.	0.34	0.48
FILTER 10	10.	24.	0.34	0.48
FILTER 11	9.	26.	0.32	0.47
FILTER 12	10.	16.	0.32	0.46
FILTER 13	11.	19.	0.29	0.40

## ----- AIR FLOW DATA -----

SITE NUMBER 1

TOTAL FLOW = 14833.7 CUBIC METERS

	FLOW 1	FLOW 2	DAYS	ALPHA CNTS	BETA CNTS
SAMPLE 1	4.0	4.0	7.	26.	89.
SAMPLE 2	4.0	4.0	7.	25.	70.
SAMPLE 3	4.0	4.0	7.	19.	66.
SAMPLE 4	4.0	4.0	7.	19.	73.
SAMPLE 5	4.0	4.0	7.	12.	70.
SAMPLE 6	4.0	4.0	7.	19.	73.
SAMPLE 7	4.0	4.0	7.	17.	93.
SAMPLE 8	4.0	4.0	7.	19.	151.
SAMPLE 9	4.0	4.0	7.	18.	166.
SAMPLE 10	4.0	4.0	7.	13.	72.
SAMPLE 11	4.0	4.0	7.	118.	142.
SAMPLE 12	4.0	4.0	7.	20.	78.
SAMPLE 13	4.0	4.0	7.	19.	48.

SITE NUMBER 2  
TOTAL FLOW = 14833.7 CUBIC METERS

	FLOW 1	FLOW 2	DAYS	ALPHA CNTS	BETA CNTS
SAMPLE 1	4.0	4.0	7.	17.	90.
SAMPLE 2	4.0	4.0	7.	17.	80.
SAMPLE 3	4.0	4.0	7.	14.	57.
SAMPLE 4	4.0	4.0	7.	15.	110.
SAMPLE 5	4.0	4.0	7.	24.	117.
SAMPLE 6	4.0	4.0	7.	29.	113.
SAMPLE 7	4.0	4.0	7.	23.	105.
SAMPLE 8	4.0	4.0	7.	29.	163.
SAMPLE 9	4.0	4.0	7.	22.	114.
SAMPLE 10	4.0	4.0	7.	16.	74.
SAMPLE 11	4.0	4.0	7.	20.	85.
SAMPLE 12	4.0	4.0	7.	16.	57.
SAMPLE 13	4.0	4.0	7.	17.	95.

SITE NUMBER 3  
TOTAL FLOW = 14833.7 CUBIC METERS

	FLOW 1	FLOW 2	DAYS	ALPHA CNTS	BETA CNTS
SAMPLE 1	4.0	4.0	7.	29.	113.
SAMPLE 2	4.0	4.0	7.	24.	99.
SAMPLE 3	4.0	4.0	7.	29.	97.
SAMPLE 4	4.0	4.0	7.	40.	223.
SAMPLE 5	4.0	4.0	7.	50.	452.
SAMPLE 6	4.0	4.0	7.	33.	111.
SAMPLE 7	4.0	4.0	7.	27.	280.
SAMPLE 8	4.0	4.0	7.	48.	526.
SAMPLE 9	4.0	4.0	7.	22.	134.
SAMPLE 10	4.0	4.0	7.	24.	98.
SAMPLE 11	4.0	4.0	7.	21.	115.
SAMPLE 12	4.0	4.0	7.	21.	86.
SAMPLE 13	4.0	4.0	7.	20.	155.

## SITE NUMBER 4

TOTAL FLOW = 14833.7 CUBIC METERS

	FLOW 1	FLOW 2	DAYS	ALPHA CNTS	BETA CNTS
SAMPLE 1	4.0	4.0	7.	29.	210.
SAMPLE 2	4.0	4.0	7.	38.	161.
SAMPLE 3	4.0	4.0	7.	29.	105.
SAMPLE 4	4.0	4.0	7.	32.	285.
SAMPLE 5	4.0	4.0	7.	59.	476.
SAMPLE 6	4.0	4.0	7.	34.	222.
SAMPLE 7	4.0	4.0	7.	31.	371.
SAMPLE 8	4.0	4.0	7.	45.	636.
SAMPLE 9	4.0	4.0	7.	33.	236.
SAMPLE 10	4.0	4.0	7.	26.	124.
SAMPLE 11	4.0	4.0	7.	44.	128.
SAMPLE 12	4.0	4.0	7.	22.	87.
SAMPLE 13	4.0	4.0	7.	17.	402.

## SITE NUMBER 5

TOTAL FLOW = 14833.7 CUBIC METERS

	FLOW 1	FLOW 2	DAYS	ALPHA CNTS	BETA CNTS
SAMPLE 1	4.0	4.0	7.	35	462.
SAMPLE 2	4.0	4.0	7.	52.	304.
SAMPLE 3	4.0	4.0	7.	47.	131.
SAMPLE 4	4.0	4.0	7.	50.	161.
SAMPLE 5	4.0	4.0	7.	105.	518.
SAMPLE 6	4.0	4.0	7.	29.	92.
SAMPLE 7	4.0	4.0	7.	29.	238.
SAMPLE 8	4.0	4.0	7.	44.	396.
SAMPLE 9	4.0	4.0	7.	43.	169.
SAMPLE 10	4.0	4.0	7.	29.	92.
SAMPLE 11	4.0	4.0	7.	31.	133.
SAMPLE 12	4.0	4.0	7.	25.	100.
SAMPLE 13	4.0	4.0	7.	57.	248.



## SITE NUMBER 6

TOTAL FLOW = 14833.7 CUBIC METERS

	FLOW 1	FLOW 2	DAYS	ALPHA CNTS	BETA CNTS
SAMPLE 1	4.0	4.0	7.	25.	387.
SAMPLE 2	4.0	4.0	7.	36.	148.
SAMPLE 3	4.0	4.0	7.	29.	92.
SAMPLE 4	4.0	4.0	7.	33.	195.
SAMPLE 5	4.0	4.0	7.	15.	109.
SAMPLE 6	4.0	4.0	7.	28.	175.
SAMPLE 7	4.0	4.0	7.	25.	326.
SAMPLE 8	4.0	4.0	7.	20.	199.
SAMPLE 9	4.0	4.0	7.	33.	549.
SAMPLE 10	4.0	4.0	7.	13.	62.
SAMPLE 11	4.0	4.0	7.	23.	220.
SAMPLE 12	4.0	4.0	7.	28.	73.
SAMPLE 13	4.0	4.0	7.	20.	311.

## SITE NUMBER 7

TOTAL FLOW = 14833.7 CUBIC METERS

	FLOW 1	FLOW 2	DAYS	ALPHA CNTS	BETA CNTS
SAMPLE 1	4.0	4.0	7.	39.	354.
SAMPLE 2	4.0	4.0	7.	37.	171.
SAMPLE 3	4.0	4.0	7.	23.	90.
SAMPLE 4	4.0	4.0	7.	28.	144.
SAMPLE 5	4.0	4.0	7.	14.	77.
SAMPLE 6	4.0	4.0	7.	34.	547.
SAMPLE 7	4.0	4.0	7.	25.	199.
SAMPLE 8	4.0	4.0	7.	9.	172.
SAMPLE 9	4.0	4.0	7.	28.	138.
SAMPLE 10	4.0	4.0	7.	21.	79.
SAMPLE 11	4.0	4.0	7.	38.	286.
SAMPLE 12	4.0	4.0	7.	14.	205.
SAMPLE 13	4.0	4.0	7.	26.	24.

## SITE NUMBER 8

TOTAL FLOW = 14833.7 CUBIC METERS

	FLOW 1	FLOW 2	DAYS	ALPHA CNTS	BETA CNTS
SAMPLE 1	4.0	4.0	7.	25.	145.
SAMPLE 2	4.0	4.0	7.	32.	111.
SAMPLE 3	4.0	4.0	7.	16.	109.
SAMPLE 4	4.0	4.0	7.	18.	80.
SAMPLE 5	4.0	4.0	7.	15.	61.
SAMPLE 6	4.0	4.0	7.	37.	226.
SAMPLE 7	4.0	4.0	7.	18.	112.
SAMPLE 8	4.0	4.0	7.	29.	153.
SAMPLE 9	4.0	4.0	7.	30.	121.
SAMPLE 10	4.0	4.0	7.	26.	80.
SAMPLE 11	4.0	4.0	7.	42.	201.
SAMPLE 12	4.0	4.0	7.	21.	152.
SAMPLE 13	4.0	4.0	7.	19.	52.

## SITE NUMBER 9

TOTAL FLOW = 14833.7 CUBIC METERS

	FLOW 1	FLOW 2	DAYS	ALPHA CNTS	BETA CNTS
SAMPLE 1	4.0	4.0	7.	20.	74.
SAMPLE 2	4.0	4.0	7.	23.	95.
SAMPLE 3	4.0	4.0	7.	29.	128.
SAMPLE 4	4.0	4.0	7.	17.	91.
SAMPLE 5	4.0	4.0	7.	17.	69.
SAMPLE 6	4.0	4.0	7.	28.	142.
SAMPLE 7	4.0	4.0	7.	20.	92.
SAMPLE 8	4.0	4.0	7.	25.	117.
SAMPLE 9	4.0	4.0	7.	33.	130.
SAMPLE 10	4.0	4.0	7.	24.	84.
SAMPLE 11	4.0	4.0	7.	81.	311.
SAMPLE 12	4.0	4.0	7.	25.	116.
SAMPLE 13	4.0	4.0	7.	17.	78.

## SITE NUMBER 10

TOTAL FLOW = 14833.7 CUBIC METERS

	FLOW 1	FLOW 2	DAYS	ALPHA CNTS	BETA CNTS
SAMPLE 1	4.0	4.0	7.	17.	59.
SAMPLE 2	4.0	4.0	7.	10.	74.
SAMPLE 3	4.0	4.0	7.	22.	96.
SAMPLE 4	4.0	4.0	7.	22.	122.
SAMPLE 5	4.0	4.0	7.	18.	88.
SAMPLE 6	4.0	4.0	7.	14.	70.
SAMPLE 7	4.0	4.0	7.	18.	80.
SAMPLE 8	4.0	4.0	7.	18.	76.
SAMPLE 9	4.0	4.0	7.	21.	65.
SAMPLE 10	4.0	4.0	7.	38.	75.
SAMPLE 11	4.0	4.0	7.	70.	266.
SAMPLE 12	4.0	4.0	7.	26.	98.
SAMPLE 13	4.0	4.0	7.	17.	44.

## SITE NUMBER 11

TOTAL FLOW = 14833.7 CUBIC METERS

	FLOW 1	FLOW 2	DAYS	ALPHA CNTS	BETA CNTS
SAMPLE 1	4.0	4.0	7.	18.	75.
SAMPLE 2	4.0	4.0	7.	30.	69.
SAMPLE 3	4.0	4.0	7.	18.	133.
SAMPLE 4	4.0	4.0	7.	19.	122.
SAMPLE 5	4.0	4.0	7.	12.	66.
SAMPLE 6	4.0	4.0	7.	18.	77.
SAMPLE 7	4.0	4.0	7.	8.	62.
SAMPLE 8	4.0	4.0	7.	11.	73.
SAMPLE 9	4.0	4.0	7.	20.	116.
SAMPLE 10	4.0	4.0	7.	21.	59.
SAMPLE 11	4.0	4.0	7.	62.	189.
SAMPLE 12	4.0	4.0	7.	15.	151.
SAMPLE 13	4.0	4.0	7.	18.	58.

## ----- COUNTS ENTERED -----

	U238	U235	U234	U232	DETECTOR	DAY
SITE NUMBER 1	78.	119.	586.	73.	1	1
SITE NUMBER 2	74.	27.	255.	54.	2	1
SITE NUMBER 3	251.	67.	861.	68.	3	1
SITE NUMBER 4	222.	65.	726.	48.	1	3
SITE NUMBER 5	401.	101.	1626.	53.	1	2
SITE NUMBER 6	345.	70.	486.	62.	2	2
SITE NUMBER 7	265.	43.	325.	47.	3	2
SITE NUMBER 8	244.	49.	288.	61.	2	3
SITE NUMBER 9	374.	57.	392.	78.	1	2
SITE NUMBER 10	254.	72.	372.	64.	2	2
SITE NUMBER 11	95.	31.	180.	31.	3	2

----- PRELIMINARY RESULTS -----  
 DISINTEGRATIONS PER MINUTE PER TOTAL FILTER

	U238	U235	U234	ALPHA	BETA
FILTER 1	2.31E+01	3.55E+01	1.70E+02	5.38E+02	1.04E+03
FILTER 2	3.01E+01	1.05E+01	9.98E+01	3.32E+02	1.13E+03
FILTER 3	8.05E+01	2.09E+01	2.72E+02	6.51E+02	2.56E+03
FILTER 4	1.02E+02	2.92E+01	3.29E+02	7.72E+02	3.71E+03
FILTER 5	1.66E+02	4.10E+01	6.70E+02	1.12E+03	3.20E+03
FILTER 6	1.22E+02	2.47E+01	1.69E+02	4.97E+02	2.98E+03
FILTER 7	1.23E+02	1.96E+01	1.44E+02	5.16E+02	2.53E+03
FILTER 8	8.76E+01	1.73E+01	1.00E+02	4.96E+02	1.52E+03
FILTER 9	1.05E+02	1.55E+01	1.06E+02	5.71E+02	1.43E+03
FILTER 10	8.66E+01	2.48E+01	1.27E+02	4.54E+02	1.07E+03
FILTER 11	6.60E+01	2.13E+01	1.20E+02	3.53E+02	1.11E+03

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 \*  
 \* AIR FILTER COMPOSITES \*  
 \*  
 \* FINAL REPORT \*  
 \*  
 \* SECOND QUARTER, 1983 \*  
 \*  
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MICROCURIES PER CUBIC CENTIMETER

<u>SITE NUMBER</u>	<u>U238</u>	<u>U235</u>	<u>U234</u>	<u>GROSS ALPHA</u>	<u>GROSS BETA</u>
1	7.02E-16	1.08E-15	5.17E-15	1.63E-14	3.15E-14
2	9.13E-16	3.18E-16	3.03E-15	1.01E-14	3.43E-14
3	2.44E-15	6.35E-16	8.26E-15	1.98E-14	7.78E-14
4	3.09E-15	8.88E-16	1.00E-14	2.35E-14	1.13E-13
5	5.05E-15	1.24E-15	2.03E-14	3.39E-14	9.71E-14
6	3.70E-15	7.51E-16	5.13E-15	1.51E-14	9.06E-14
7	3.74E-15	5.94E-16	4.38E-15	1.57E-14	7.68E-14
8	2.66E-15	5.26E-16	3.04E-15	1.51E-14	4.60E-14
9	3.20E-15	4.71E-16	3.22E-15	1.73E-14	4.36E-14
10	2.63E-15	7.52E-16	3.86E-15	1.38E-14	3.24E-14
11	2.00E-15	6.47E-16	3.64E-15	1.07E-14	3.38E-14
DETECTION LIMITS:	3.87E-17	5.38E-17	1.31E-16	2.09E-16	2.19E-16

EQUATIONS USED IN THIS REPORT:

DETECTION LIMIT =  $(2 * (\text{BACKGROUND} ** 0.5)) / \text{AVG FLOW PER SITE}$

ISOTOPIC CONC. =  $(\text{NET CNTS.} / \text{TIME} / \text{EFF} / \text{REC}) - (\text{NET SAM BLK CNTS.} / \text{TIME} / \text{EFF} / \text{REC})$

GROSS CONC. =  $\text{NET CNTS.} / \text{TIME} / \text{EFF} / \text{PAPER FCTR.}$

FLOW = SUMMATION:  $\text{AVG FLOW} * 0.0283 \text{ M}^{**3} / \text{FT}^{**3} * \text{DAYS} * 1440 \text{ MIN} / \text{DAY} * 10\text{E}6 \text{ CM}^{**3} / \text{M}^{**3}$

ALL VALUES WERE MULTIPLIED BY 2 TO ACCOUNT FOR THE TOTAL FILTER.

THESE VALUES WERE CHECKED AND APPROVED BY \_\_\_\_\_.

## DISTRIBUTION

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